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Technological and Theoretical Challenges in Oxy-Fuel Combustion

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Climate Change & Combustion

Two Outstanding Issues

♦Oxy-Fuel Combustion for CCS ▶CCS = CO₂ Capture & Storage

Climate Forcing By Black Carbon Particularly on the Arctic Climate



Numerical Modelling ?

- Numerical Prediction
- Numerical Model
- Numerical Computation
- Numerical Simulation
- *CFD



Are They the Same ?



What is Modelling ?

- Modelling
 - ➢ Simplify
 - The Complex Real-World Problems
 - ➤To a Tractable Form
 - ➤While Maintaining the Physical Essence
- Modelling Procedure
 - ➢ Physical Modelling
 - Mathematical (or Experimental) Modelling
 - ➢Numerical (or Experimental) Realization



Contents

What is Oxy-Fuel Combustion ?

• Applications

Physical Essence of Oxy-Fuel Combustion

• Theoretical Challenges

Mathematical Modelling Issues

Technological Challenges



What is Oxy-Fuel Combustion ?

Stoichiometry \rightarrow Oxy-Fuel : CH₄ + 2O₂ \rightarrow CO₂ + 2H₂O \rightarrow Air-Fuel : CH₄ + 2(O₂+3.76N₂) \rightarrow CO₂ + 2H₂O + 7.52N₂

Higher Flame Temperature (~ 3000K)

Improved Heat Transfer & Thermal Efficiency

- Enhanced Heat Transfer ← High Temperature & Concentrations of CO₂ and H₂O
- Less Energy-Loss through Exhaust Gas
- Need to Overcome the Oxygen Production Cost

Significant Increase in Flame Stability

Easy to Capture CO₂



Oxy-Fuel Combustion

♦ Where do we use it ?

| Application | Why ? |
|-----------------------------------|---|
| Industrial Furnace | Higher Thermal Efficiency Higher Productivity |
| Gasification or Fuel Reforming | Rich Oxy-Fuel Combustion Maintaining the Gasifying Reaction |
| Oxy-PC Combustion with FGR | CO₂ Capture <u>Retrofitting</u> the Existing PC Power Plant |
| Oxy-PC Combustion w/o FGR | CO₂ Capture High Performance CCS-Capable PC Power Plant Only Conceptually Exists |



OFC for Industrial Furnace

- ✤ Mainly For Metal Heating & Glass Melting
- ✤ High Exit Temperature > 1000K
 - \succ Air-Fuel Flame : T_f < 2000K → η < 50%
- Oxy-Fuel Flame Temperature ~ 3000K : η ~ 70%
- Low NOx, Higher Productivity and Quality
- Enough to Cover the Oxygen Cost



Source : Oxygen-Enhanced Combustion (CRC Press)



OFC Gasifier



Elcogas IGCC Gasifier

♦ Gasification by Partial Oxidation > C + $\frac{1}{2}$ O₂ → CO

Rich Oxy-Fuel Combustion

Pure Oxygen to Maintain the Reaction Temperature





OFC for PC Power Plant





Physical Essence

Chemical Kinetics

Flame Structure

Heterogeneous Combustion



Chemistry

| ••• | Radica | ls |
|-----|--------|----|
| | | |

- Chain Branching
 - ♦ 1 : $O_2 + H \rightarrow OH + O$
- Radical Recombination

$$\blacklozenge 5 : O_2 + H + M \rightarrow HO_2 + M'$$

- Crossover Temperature
 - $\bullet \ \omega_1 = \omega_5$
- Methane oxidation
 - Fuel decomposition
 - $\blacklozenge CH_4 + 1.5O_2 \rightarrow CO + H_2O$
 - Dominated by reaction #1
 - ♦ 11 : $CH_4 + H \rightarrow CH_3 + H_2$
 - CO oxidation
 - \diamond CO + 0.5O₂ \rightarrow CO₂
 - Dominated by reaction #10
 - ◆ 10 : CO +OH \rightarrow CO₂ + H

| | Step | | Reac | tion | <i>B</i> * | α* | E^* | |
|---|-------|-----------------------|---------------|---|----------------------------------|-----------------|--------|----------|
| | 1 | $O_2 + H$ | \rightarrow | OH + O | 2.00 10 ¹⁴ | 0.00 | 70.30 | -7 |
| / | 1b | OH + O | \rightarrow | $O_2 + H$ | 1.40 1013 | 0.00 | 3.20 | _ |
| | 2 | $O + H_2$ | \rightarrow | H + OH | 1.50 107 | 2.00 | 31.60 | |
| | 2b | H + OH | \rightarrow | $O + H_2$ | 6.73 10 ⁶ | 2.00 | 22.35 | |
| | 3 | $OH + H_2$ | \rightarrow | $H + H_2O$ | 1.00 10 ⁸ | 1.60 | 13.80 | |
| | 3b | $H + H_2O$ | \rightarrow | $OH + H_2$ | 4.62 108 | 1.60 | 77.50 | |
| | 4 | OH + OH | \rightarrow | $H_2O + O$ | 1.50 109 | 1.14 | 0.42 | |
| | 4b | $H_2O + O$ | \rightarrow | OH + OH | 1 49 10 ¹⁰ | 1.14 | 71.14 | |
| | 5** | $H + O_2 + M$ | \rightarrow | $HO_2 + M$ | 2.30 1018 | -0.80 | 0.00 | ~ 1 |
| 1 | 6 | $HO_2 + H$ | \rightarrow | OH + OH | 1.50 1014 | 0.00 | 4.20 | |
| / | 7 | $HO_2 + H$ | \rightarrow | $H_2 + O_2$ | 2.50 1013 | 0.00 | 2.90 | |
| | 8 | $HO_2 + H$ | \rightarrow | $H_2O + O$ | 3.00 1013 | 0.00 | 7.20 | |
| | 9 | $HO_2 + OH$ | | H20+02 - | 2.00 +013 - | - 0.00- | 7.20 | |
| | 10 | CO + OH | \rightarrow | $CO_2 + H$ | 4.40 10 ⁶ | 1.50 | -3.10 | 1 |
| | 10b | - CO ₂ + H | - | $CO \rightarrow OH$ | -4 .96 10⁸ | 1.50 | -89.71 | |
| 1 | 11 | $CH_4 + H$ | \rightarrow | $H_2 + CH_3$ | 2.20 10 ⁴ | 3.00 | 36.60 | |
| | 11b | $H_2 + CH_3$ | \rightarrow | $CH_4 + H$ | 8.83 10 ² | 3.00 | 33.53 | |
| | 12 | $CH_4 + OH$ | \rightarrow | $H_2O + CH_3$ | $1.60 \ 10^{6}$ | 2.10 | 10.30 | |
| | 13 | $CH_3 + O$ | \rightarrow | $CH_2O + H$ | 7.00 1013 | 0.00 | 0.00 | |
| / | 14 | $CH_3 + OH$ | \rightarrow | $\mathrm{CH}_{2}\mathrm{O} + \mathrm{H} + \mathrm{H}$ | 9.00 1014 | 0.00 | 64.80 | |
| | 15 | $CH_3 + OH$ | \rightarrow | $CH_2O + H_2$ | 8.00 1012 | 0.00 | 0.00 | |
| | 16*** | $CH_3 + H$ | \rightarrow | CH ₄ | 6.00 1016 | -1.00 | 0.00 | |
| | 17 | $CH_2O + H$ | \rightarrow | $CHO + H_2$ | 2.50 1013 | 0.00 | 16.70 | |
| | 18 | CH ₂ O+OH | \rightarrow | $CHO + H_2O$ | 3.00 1013 | 0.00 | 5.00 | |
| | 19 | CHO + H | \rightarrow | $CO + H_2$ | $2.00 \ 10^{14}$ | 0.00 | 0.00 | |
| | 20 | CHO + OH | \rightarrow | $CO + H_2O$ | 1.00 1014 | 0.00 | 0.00 | |
| | 21 | $CHO + O_2$ | \rightarrow | $CO + HO_2$ | 3.00 1012 | 0.00 | 0.00 | |
| | 22** | CHO + M | \rightarrow | CO + H + M | 7.10 1014 | 0.00 | 70.30 | |
| | 23 | $CH_3 + H$ | \rightarrow | $CH_2 + H_2$ | $1.80 \ 10^{14}$ | 0.00 | 63.00 | |
| | 24 | $CH_2 + O_2$ | \rightarrow | $\rm CO_2 + H + H$ | 6.50 10 ¹² | 0.00 | 6.30 | |
| | 25 | $CH_2 + O_2$ | \rightarrow | CO + OH + H | 6.50 1012 | 0.00 | 6.30 | |
| | 26 | $CH_2 + H$ | \rightarrow | $CH + H_2$ | 4.00 10 ¹³ | 0.00 | 0.00 | |
| | 26b | $CH + H_2$ | \rightarrow | $CH_2 + H$ | 2.79 1013 | 0.00 | 12.61 | |
| | 27 | $CH + O_2$ | \rightarrow | CHO + O | 3.00 1013 | 0.00 | 0.00 | |
| | 28 | $CH_3 + OH$ | \rightarrow | $CH_2 + H_2O$ | 1.50 1013 | 0.00 | 20.93 | |
| | 29 | $CH_2 + OH$ | \rightarrow | $CH_2O + H$ | 2.50 1013 | 0.00 | 0.00 | |
| | 30 | $CH_2 + OH$ | \rightarrow | $CH + H_2O$ | 4.50 1013 | 0.00 | 12.56 | |
| | 31 | CH + OH | \rightarrow | CHO + H | 3.00 1013 | 0.00 | 0.00 | |

* Here cm, mol, K and kJ are the units.

** Catalytic efficiencies differ for different M; values here are for $M = H_2$. *** The high-pressure value k_{∞} is given here; tail-off curves are $k/k_{\infty} = (1 + 21.5 \times 10^{10} T^3/p^{0.6})^{-1}$, where p is in atm and T in K.

A. Liñán and F. A. Williams

Fundamental Aspects of Combustion, 1993, p.50



4-Step Mechanism

| Fuel C | Consu | mption | |
|--|---------------------------------|--------------------------------|--------------|
| $CH_4 + H$ | \rightarrow | $\mathrm{CH}_3 + \mathrm{H}_2$ | |
| $CH_3 + O$ | \rightarrow | $CH_2O + H$ | |
| $CH_2O + H$ | \rightarrow | $CHO + H_2$ | |
| CHO + M | \rightarrow | CO + H + M | |
| H + OH | \rightarrow | $\mathrm{O}+\mathrm{H}_{2}$ | |
| $H + H_2O$ | \rightarrow | $OH + H_2$ | |
| $\mathrm{CH}_4 + \mathrm{2H} + \mathrm{H}_2\mathrm{O}$ | \rightarrow | $\rm CO + 4H_2$ | |
| Wate | r-Ga | s Shift | |
| CO + OH | \rightleftharpoons | $CO_2 + H$ | |
| $H + H_2O$ | \rightleftharpoons | $OH + H_2$ | |
| $CO + H_2O$ | \rightleftharpoons | $CO_2 + H_2$ | |
| Reco | mbin | ation | |
| $O_2 + H + M$ | \rightarrow | $HO_2 + M$ | |
| $OH + HO_2$ | \rightarrow | $H_2O + O_2$ | |
| $H + H_2O$ | \rightarrow | $OH + H_2$ | |
| 2H + M | \rightarrow | $H_2 + M$ | |
| Oxygen Co | onsui | nption and | |
| Radica | l Pro | duction | |
| $O_2 + H$ | \rightleftharpoons | OH + O | |
| $O + H_2$ | \rightleftharpoons | OH + H | |
| $OH + H_2$ | \rightleftharpoons | $H_2O + H$ | |
| $OH + H_2$ | $\stackrel{\longrightarrow}{=}$ | $H_2O + H$ | |
| $O_2 + 3H_2$ | ~`` | $2H_2O + 2H$ | A. Liñán and |

A. Liñán and F. A. Williams Fundamental Aspects of Combustion, 1993, p.51



Flame Structure

Air-Fuel Flame



Oxy-Fuel Flame





CF124:295-310 Kennedy (Illinois Chicago)

· , Tmax SP 1.2 3000 CH, 2500 0.8 Molar fractions 2000 0, 1500 🔀 Crossover temperature 0.4 но 1000 500 0 0 0.5 1.5 2 Distance from the fuel nozzle, cm

(b)

Korea Institute of Science and Technology

Two-Zone Structure

Thin "fuel decomposition region"

• Similar structure to the premixed flame of CH₄ and radicals

Thick "CO oxidation region"



>CH₄-R Premixed Flame
 >Super-Adiabatic Downstream
 >AEA by Linan
 →No Extinction
 →Improved Flame Stability



Robust Flame

Thin Fuel Decomposition Layer

• No Quenching **←** Superadiabatic

Thick CO Oxidation Layer

- $\delta_{\text{Oxy-Fuel}} \gg \delta_{\text{Air-Fuel}}$
- Longer Residence Time : t_{Diff} ~ δ^2
- Higher Temperature → Shorter Chemical Time t_{Ch}

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- t_{Diff} >> t_{Ch} → Extremely Difficult to Quench
- Providing the Superadiabatic Thermal Shield

Fuel Reforming

Thinner CO Oxidation Layer

- Less Thermal Shielding for the Fuel Decomposition Layer
- Much Weaker to Outer Disturbances

What Happens if the Fuel Decomposition Layer is Percolated ?

- Can Occur for Heterogeneous Combustion
 - Fuel : Pulverized Coal or Heavy Fuel Oil
- Partial Oxidation vs Partial Combustion ?



Heterogeneous Combustion

- Percolated by Fuel Spray
- Partial Combustion
 - Completely Burnt or Unburnt
- Poor Gasification



- Percolated but Self-Healed
 - Repaired by Strong Reaction Structure
- Complete Combustion or Gasification
- Key Issue : Prevention of the Fuel-Decomposition Reaction-Front Percolation



Numerical Modelling

Transport : Strong Turbulence

- Oxy-Fuel Burner ~ Simple Co-Axial Pipes
- High Injection Velocity
 - Better Burner Tip Cooling
 - Better Recirculation Region → Better NOx Control
 - Improved Heat Transfer Properties

Kinetics : Thin Flame or Distributed Reaction ?

• Flamelet Model , CMC , PDF ,



CMC Calculation Results

Velocity and Mixture Fraction Fields





CMC Calculation Results

Temperature Fields

IFRF-Burner A



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Inaccuracies in the Boundary Condition & Conditioned Moments

Difficulties in Numerical Modelling

Limited Benchmarking Data

- No Turbulent Flame Structure Data
 - Lack of DNS Data & Optical Visualization or Measurements
- Limited Industrial Furnace Measurement
 - Incomplete Bench Marking Data from IFRF

Choice of Model

- Flame Thickness → Chemistry Closure (Flamelet or CMC)
- Strong Turbulence → Inaccuracy of Conditioned Moments

Yet Premature for Parametric Studies



Technical Challenges

OFC in Industrial Furnaces

• Most Technical Problems Are Solved or Solvable.

Gasification

- Occurrence of Partial Combustion
- Extremely Difficult for Numerical Modelling

OFC for CCS

- Uncertainties in the Retrofit Routes
- High CCS Cost → Increase in your electricity bill
 - Low Efficiency → High Fuel Cost
 - More Equipment → High Initial Investment



Difficulties in Gasification

- Consulting Inquiry from Samsung-BP
 - Gasification of HFO to Produce CO
 - Gasifier from GE-Energy (Chevron-Texaco)
- Problems
 - → Higher CO_2 Concentration ? → Yes !
 - ➤ Higher Soot Formation ? → Yes !
 - ➢ Flame Instability ? → Yes !
 - ♦ Burner Tip Was Damaged
- Cause
 - ➢ Burner Tip Damage → Loss of Stability
 - → Partial Quenching of Fuel Decomposition Layer
 - → Partial Combustion (CO2 & Soot Formation)
 - ➔ More Heat Loss ➔ More Partial Combustion
 - ➔ Failure of Partial Oxidation



Samsung-BP Case

- ✤ What Do They Want ?
 - Numerical Simulation of Unsatisfactory Gasification & Find a Remedy
- My Answer
 - ➢ No Way to do the Correct Numerical Simulation
 - No Subgrid Model for Partial Combustion
 - Partial Quenching of Thin Fuel-Decomposition Layer
- They Are Still Looking for Someone Who Can Do the Numerical Work.
- ✤ BAD Example Not to Follow
 - Numerical Modelling (?) without Physical Understanding



Samsung-BP Case

- How to Solve the Problem
- Fuel Preparation
 - Preheating to Improve Atomization
 - Steam Injection : Adding H & O
- Burner Design
 - Better Thermal Cooling for the Tip
 - Increase Injection Speed (Smaller Diameter ?)

Cheap Burner Design: Easy to Exchange

Optimize the Burner & Furnace Shapes



Oxy-PC Modelling Issue

Combustion with FGR

- Similar to Air Combustion : $N_2 \rightarrow CO_2$
- Doable with the Current Numerical Model

Radiative Heat Transfer

- New Castle Group : Stronger Radiation by CO₂
- Utah Group : No Significant Modification for Radiation
 - Radiation Dominated by Particles
- Others
 - We Need More Research to Figure Out Who's Correct.



CCS Cost (Retrofitting)

| Coal Power Generation Cost | | | | | |
|--|---------|--------|--|--|--|
| Base COE (before CCS) | | 5¢/kWh | | | |
| CCS Investment Cost | +1¢/kWh | 6¢/kWh | | | |
| CCS Energy Consumption ➢ Efficiency : 40% → 30% → Less Electricity to Sell | X 4/3 | 8¢/kWh | | | |

- ✤ Over 50% Electricity Whole Sale Price Increase
- More Power Plants & Coal Consumption are Needed
- Higher Cost Rise for Lower Efficiency Plants
- There are Other Hidden Costs too.
- Likely Double the COE



CCS Cost

✦How to Reduce the CCS Cost ➢ Improve Power Plant Efficiency ➢ Reduce Fuel Cost ➢ Reduce Equipment Cost



CCS @ Power Industry



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Future CCS Technology

Placement

- Another Dark Age of Nuclear Power ?
- More PC Power Demand (Base Load Coverage)
- Sorry! Renewable Energy Cannot Meet the Baseline Power Demand.
- \rightarrow CCS Becomes the Primary Route to Reduce CO₂ Emission

Basic Requirements

- High Efficiency : 700+°C Steam Temperature $\rightarrow \eta > 50\%$
- Low Plant Cost : Simple & Compact Power Plant Design
- Fuel Flexibility : Lower Fuel Cost
- Easy CO₂ Capture



Basic Requirements





Possibilities

Cyclone Furnace Oxy-Coal Combustion

- ≻ Recommended by KT, BL
- ♦ CFBC ?
 - Flow Rate may be too Low
 - ➤ Any Possibilities ?
- ✤IGCC ?
 - Economically Competitive ?
 - Unlikely Against Oxy-Coal
- Any Likely Option for PCC Route ?
 - > PCC = Post-Combustion Capture





Theoretical Challenges

Need to Verify the Two-Zone Structure for Turbulent Oxy-Fuel Flames

- By DNS
- & Optical Diagnostics
- Chemistry Modelling
 - Thin Flame or Distributed Reaction ?
- Transport Modelling
 - Handling of the High Turbulence by High-Speed Injection.

Industrial Simulation

Need Good Benchmark Data for Code Tuning

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Technological Challenges

Oxy-Fuel Combustion in General

➢ Robust Flame → Less Technical Difficulties

Gasification or Fuel Reforming

- Insufficient Understanding of Reaction Zone Structure
- Prevention of Partial Combustion
- How to Maintain the Integrity of the Fuel-Decomposition Reaction Front

***** Oxy-PC for CCS

- Development of High Efficiency CCS-Ready Power Plant
- Technological Doable
- Financially Doable ?

